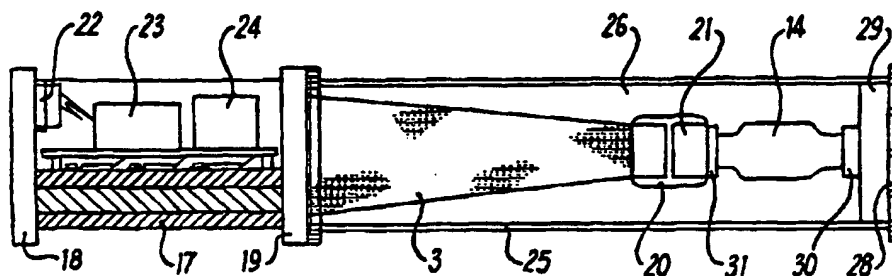




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<p>(21) International Application Number: PCT/GB94/02087</p> <p>(22) International Filing Date: 26 September 1994 (26.09.94)</p> <p>(30) Priority Data: 9319867.9 27 September 1993 (27.09.93) GB</p> <p>(71) Applicant (for all designated States except US): EAGLE LCS LIMITED [GB/GB]; NDT House, Bridge Street, Montrose DD10 8AJ (GB).</p> <p>(72) Inventors; and (75) Inventors/Applicants (for US only): McGUIRE, Francis, William [GB/GB]; 27 Castle Crescent, Inverbervie, Montrose DD10 0SB (GB). DEVLIN, Brian [GB/GB]; Craighall, Victoria Terrace, Inverbervie, Montrose DD10 0PS (GB).</p> <p>(74) Agent: McCALLUM, Graeme, David; Murgitroyd & Company, 373 Scotland Street, Glasgow G5 8QA (GB).</p>	<p>(81) Designated States: AM, AT, AU, BB, BG, BR, BY, CA, CH, CN, CZ, DE, DK, ES, FI, GB, GE, HU, JP, KE, KG, KP, KR, KZ, LK, LT, LU, LV, MD, MG, MN, MW, NL, NO, NZ, PL, PT, RO, RU, SD, SE, SI, SK, TJ, TT, UA, US, UZ, VN, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG), ARIPO patent (KE, MW, SD, SZ).</p> <p>Published <i>With international search report. Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i></p>	

(54) Title: A MOBILE X-RAY UNIT



(57) Abstract

A mobile X-ray unit (36) is described. The unit (36) includes a low voltage direct current power supply (1), an inverter (2) coupled to the power supply (1) and a rectifier (3) coupled to the inverter (2). The inverter (2) converts the low voltage direct current from the power supply (1) to alternating current and the rectifier (3) converts the alternating current to high voltage direct current. An X-ray source (14) is also provided which is energized by the high voltage direct current from the rectifier (3). The unit (36) also has coupling means (24) to permit the unit (36) to be coupled to a translation means (33) which propels the unit (36). The unit (36) is particularly useful for insertion into a tubular member for non-destructive testing of the tubular member.

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1 "A Mobile X-Ray Unit"

2 This invention relates to X-ray units, and in
3 particular, but not exclusively, for non-destructive
4 testing (N.D.T.).

5 When steel has been fabricated, it is desirable, and
6 frequently mandatory, that the steelwork and/or welds
7 therein be subjected to non-destructive testing
8 (N.D.T.) to verify the integrity of the steelwork
9 and/or welds. In the case of pipes, tubes and ducts,
10 N.D.T. equipment may be inserted into the bore of the
11 pipe or other tubular article on a mobile unit known as
12 a "pig" or a "pipe crawler" (hereinafter collectively
13 referred to as a "crawler"). A common form of N.D.T
14 involves X-raying of the articles under test. Use of a
15 gamma source for the generation of X-rays has the
16 disadvantages of being a permanent radiation hazard,
17 and of being subject to special regulatory controls.
18 Electrical generation of X-rays overcomes some of the
19 hazards of radio-isotopes, but conventional
20 electrically-powered X-ray sources have their own
21 disadvantages, as will now be detailed.

22 Past and present X-ray crawlers have been designed and

1 built around an X-ray tube. These tubes are usually of
2 the half-wave self-rectifying low-frequency type which
3 work on 50-60 Hz chopped battery or direct AC volts
4 into a large step up transformer (120V DC in =160,000V
5 AC out), have not changed in design in almost forty
6 years, and are the only type of X-ray tubes currently
7 available for use with crawlers or mobile use.

8 The existing tube rectifies on each half of the
9 positive cycle 0-160 kV, then back to 0 kV. The purity
10 of the subsequent X-ray beam output suffers as a result
11 of this inefficient process. If radiography requires
12 140 kV to produce a film, then a substantial part of
13 0-140 kV-0 produced is wasted energy. The efficiency
14 of this type of unit is less than 10%. This has always
15 been accepted by industry as the standard because, to
16 date, it has not been possible to produce X-rays in any
17 other form that is portable or for crawlers.
18 Constant-potential radiography has always been reserved
19 for expensive equipment laboratories and hospitals in
20 which the equipment is not intended to be portable.
21 The high cost and size of constant-potential units have
22 also been an inhibiting factor as regards development
23 of a portable unit. For example, a typical
24 conventional 160 kV constant-potential X-ray tube would
25 fill an 8' x 8' area with oil tanks and high voltage
26 generators.

27 At present all "portable" X-ray sets are very bulky,
28 heavy and require a generator to power the unit. The
29 X-ray head will typically weigh in excess of 55kg.
30 This is due to the requirement of a very large
31 transformer in the head together with cooling oil and a
32 steel case for strength. The control panel also weighs

1 about 40kg and requires 120V AC - 240V AC at 50/60Hz.

2 The disadvantages of current X-ray technology are:-

3 (i) Weight: the large battery packs that are
4 required to drive the already bulky system
5 compound the problem by adding more weight to
6 the system. The sheer weight makes
7 manoeuvrability a problem.

8 (ii) Dangerous Voltages: the 120V DC batteries
9 currently used are potentially dangerous in
10 that they can cause shock or severe burning.

11 (iii) Relay Usage: the inherent problem with
12 present-day relay usage is the high voltage
13 used. This generates sparks across the
14 contacts which, in turn, creates a burning
15 effect.

16 In accordance with a first aspect of the invention a
17 mobile X-ray unit for insertion into a tubular member
18 to irradiate the tubular member with X-rays, comprises
19 a low voltage direct current power supply; an inverter
20 coupled to the power supply, the inverter converting
21 the low voltage direct current from the power supply to
22 alternating current; rectifier means coupled to the
23 inverter, the rectifier converting the alternating
24 current to high voltage direct current; and an X-ray
25 source coupled to the rectifier to receive the high
26 voltage direct current from the rectifier to generate
27 X-rays; and coupling means to couple the unit to
28 translation means which propels the unit within the
29 tubular member.

1 Preferably, the translation means is in the form of a
2 crawler unit which propels the X-ray unit within the
3 tubular member.

4 Typically, the tubular member is a pipe, tube or duct
5 which is preferably metallic.

6 According to a second aspect of the present invention,
7 there is provided a power supply for an X-ray set, said
8 power supply comprising an inverter means, d.c. (direct
9 current) supply means for supplying d.c. to said
10 inverter means for conversion of said d.c. to a.c.
11 (alternating current), and rectifier means coupled to
12 receive said a.c. from said inverter means, said
13 inverter means functioning in use to convert said a.c.
14 to h.v.d.c. (high voltage d.c.) suitable for energising
15 an X-ray source.

16 Said inverter means is preferably a
17 pulse-width-modulated high-frequency oscillator.
18 Coupling means coupling a.c. from said inverter means
19 to said rectifier means may comprise an e.h.t (extra
20 high tension) transformer converting said a.c. from
21 said inverter means to high voltage a.c. having a
22 square-wave voltage waveform, the coupling means
23 preferably further comprising one or more
24 series-connected chokes between said inverter means and
25 said e.h.t transformer.

26 In accordance with a third aspect of the invention, a
27 rectifier for an X-ray unit comprises a number of
28 capacitors, a number of diodes coupled across the
29 capacitors, and a number of resistors coupled in series
30 to the capacitors and diodes, the capacitors, diodes

1 and resistors being encapsulated in an insulating
2 solid.

3 The rectifier may comprise a multiplier rectifier,
4 preferably a Cockroft-Walton ladder network. Said
5 multiplier rectifier preferably comprises a feedback
6 tapping intermediate the input and the output of said
7 multiplier rectifier, whereby to provide a measure of
8 the high voltage direct current (h.v.d.c) without
9 directly tapping the output of the multiplier
10 rectifier.

11 Preferably, the insulating solid may be a resin, such
12 as an epoxy resin. Typically, the resin may include a
13 filler to enhance the dielectric strength of the solid.
14 The filler may comprise alumina. Preferably, the
15 insulating solid does not suffer substantially from
16 long term degradation due to temperatures of up to
17 100°C.

18 The direct current power supply preferably comprises a
19 direct current regulator means operable to receive an
20 input direct current of relatively widely variable
21 voltage, and to deliver an output direct current to
22 said inverter means at a relatively constant voltage.
23 The regulator means preferably comprises means for
24 receiving feedback signals from the rectifier means,
25 the feedback signals representing the output voltage
26 and/or the output current of the rectifier means, the
27 regulator means preferably functioning automatically in
28 response to the feedback signals to vary the output
29 thereof in a sense which tends to diminish variations
30 of the h.v.d.c from demanded levels thereof.

1 In accordance with a fourth aspect of the invention, an
2 X-ray unit comprises an X-ray source having a cathode
3 and an anode, wherein the cathode is earthed and a low
4 voltage direct current heater current is applied to the
5 cathode, and a high voltage direct current is applied
6 to the anode.

7 The X-ray source is preferably an evacuated thermionic
8 device wherein X-rays are generated in use by the
9 impact of electrons on an anode maintained at high
10 voltage with respect to a thermionic source of the
11 electrons electrically connected as the cathode of the
12 device.

13 According to a fifth aspect of the present invention,
14 there is provided an n.d.t X-ray set for the
15 non-destructive testing of pipes, tubes, ducts and the
16 like by means of X-rays sourced therein, said X-ray set
17 being in the form of a pipe crawler, said crawler
18 comprising a wheeled trolley dimensioned to fit within
19 the bore of the pipe, tube, duct or the like, and to be
20 controllably mobile along said bore, said trolley
21 mounting an X-ray set in accordance with the second
22 aspect of the present invention.

23 An example of a mobile X-ray unit in accordance with
24 the invention will now be described with reference to
25 the accompanying drawings, in which:-

26 Fig. 1 shows a graph of penetration of X-rays from
27 a chopped DC power supply;
28 Fig. 2 shows a graph of penetration of X-rays from
29 a constant potential power supply;
30 Fig. 3 is a schematic block diagram of the

1 electronic components of an X-ray power supply;
2 Fig. 4 is a side view showing the physical
3 construction of the power supply of Fig. 3;
4 Fig. 5 is a side view similar to Fig. 4, but with
5 the multiplier and X-ray tube enclosed;
6 Fig. 6 is a side view of a crawler unit;
7 Fig. 7 is a side view of a battery unit; and,
8 Fig. 8 is a side view of a retrieval unit.

9 Practical objectives of the X-ray unit described below
10 are:-

11 (i) To introduce an X-ray tube, using switch mode
12 high frequency generators to produce a
13 constant potential regulated panoramic X-ray
14 beam.

15 (ii) To power the unit with a 24V DC battery pack.

16 Figs. 1 and 2 show penetration charts of depth of
17 penetration into a 12" steel pipe for a conventional
18 chopped DC X-ray unit and a constant potential unit,
19 respectively. In both cases the voltage is 160kV at a
20 current of 5mA.

21 The constant potential tube used has the following
22 characteristics:

- 23 (i) small;
- 24 (ii) lightweight;
- 25 (iii) robust;
- 26 (iv) low cost;
- 27 (v) achieves 75-85% efficiency;
- 28 (vi) is capable of producing laboratory results

1 on-site with portable crawlers.

2 A specification and description for a 800W, 160kV high
3 voltage power supply for an X-ray generator now
4 follows.

5 The system comprises three basic functional blocks (see
6 Fig. 3). These are:

- 7 (i) a boost section 1,
- 8 (ii) an inverter 2, and
- 9 (iii) a high voltage multiplier rectifier 3.

10 In addition, incoming power passes through an RFI
11 filter 13 before entering the boost section, and a EHT
12 transformer 4 provides an interface between the
13 inverter 2 and the multiplier 3. Boost section
14 electronics 12, inverter control electronics 9 and main
15 control electronics 11 are also provided.

16 The boost section 1 is used to allow compatibility
17 between 24V and 120V input versions by converting input
18 voltages of 24V up to a nominal 120V. The boost
19 section 1 automatically distinguishes between 24 and
20 120v supplies.

21 The inverter 2 is a pulse-width-modulated
22 high-frequency oscillator of standard design adapted to
23 suit the appropriate power levels. The output from
24 this is fed via series chokes to the transformer 4
25 where it is stepped up to a variable amplitude square-
26 wave for driving the multiplier 3.

27 The high voltage multiplier 3 is based on a

1 conventional Cockroft-Walton ladder and increases the
2 voltage to 160kV, indicated as EHT output 5 in Fig. 3.

3 The EHT output 5 is controlled using a partly closed-
4 loop system 6. The closed loop system 6 comprises a
5 current feedback line 7 and a voltage feedback line 8
6 coupled to the invertor control electronics 9. The
7 invertor control electronics 9 is coupled by line 10 to
8 the main control electronics 11. To avoid the
9 necessity of a chain of resistors to the EHT output,
10 the voltage at the third stage of the multiplier is
11 maintained at the demand level. The effect of this is
12 that when the output load increases, the EHT output 5
13 also increases proportionately. This may be
14 compensated to good precision by the addition of a
15 surge-limiting resistor (not shown) in series with the
16 output 5.

17 The physical construction of the unit is shown in Figs.
18 4 and 5 which also include an X-ray tube 14. The main
19 electronics, with the exception of the multiplier (or
20 high voltage ladder) 3, are mounted on a platform 15
21 which is bolted by bolts 16 to a heat sink assembly 17.
22 The heat sink assembly 17 is mounted between two plates
23 18, 19 and the multiplier 3 is mounted to the opposite
24 side of plate 19 from the heat sink assembly 17.

25 The multiplier 3 comprises a Cockroft-Walton ladder
26 comprising diodes, capacitors and resistors
27 encapsulated in an epoxy resin with an alumina filler.
28 The alumina helps increase the dielectric strength of
29 the encapsulation material. The encapsulation material
30 preferably may withstand temperatures of up to 100°C
31 without suffering substantial long term degradation.

1 Coupled to the end of the multiplier 3 opposite plate
2 19, is a voltage stress shredder 20 and a thermal tube
3 contact 21. Anode end 31 of the tube 14 is mounted on
4 the contact 21.

5 Attached to plate 18 is a 24-way connector 22 which is
6 connected to the RFI filter 13 in the electronics. The
7 electronics on the platform 15 consist of a power
8 supply unit 23 which comprises the RFI filter 13, boost
9 section 1, inverter 2 and transformer 4, and a control
10 unit 24 which comprises the control electronics 9, 10,
11 12.

12 Fig. 5 shows the multiplier 3 and tube 14 encased in a
13 metal cylinder 25 which is filled with a
14 coolant/isolator 26 which is in the form of a gas.
15 Typically, the gas may be sulphur hexafluoride, known
16 as SF₆. The metal cylinder 25 bolts directly on to the
17 plate 19 using holes 27 in the plate 19. The cylinder
18 25 has an end plate 28 with an insert 29 in which
19 cathode end 30 of the tube is coupled.

20 Specification of the X-ray unit is as follows:-

21 (i) Input requirements: 20V to 24V DC at
22 approximately 45 to 50
23 Amps, or 100V to 140V DC
24 at 9 to 10 Amps,
25 depending on load.
26 Automatic supply
27 detection is
28 incorporated.

29 (ii) control signals: TTL compatible high

1 voltage (HV) ON/OFF
2 control. Logic "0"= ON.
3 TTL compatible HV OK
4 signal. Logic "0"=OK.
5 Basic diagnostic function
6 active when HV active.
7 Demand signal. Ground
8 referenced 0 to + 5V
9 signal. 5-V represents
10 160KV. Accuracy better
11 than 2.5% target at 5mA
12 load.
13 Current monitor. Ground
14 referenced 0 to + 5V
15 signal where 5V
16 represents 5mA HT
17 current. Accuracy better
18 than 2.5% target.

19 (iii) Output voltage: 0 to + 160kV proportional
20 to demand signal.
21 Current load 0 to 5mA.
22 Ripple voltage <2.5% peak
23 to peak target at 60 kHz.
24 Regulation <2.5% target
25 zero to full load and <1%
26 over supply range.

27 An advantage of the unit described above is that it
28 uses a common cathode arrangement. Hence, the diodes
29 in the Cockroft-Walton ladder are inverted. The common
30 cathode arrangement has the advantage that it permits
31 direct control of the heater on the cathode and does
32 not have the problems associated with isolation of the

1 heater voltage and the high voltage of 160kV.

2 Although the example described above is for a 160kV
3 unit other voltage units could be designed by making
4 appropriate changes to the power supply unit and
5 control electronics.

6 Fig. 6 shows the apparatus of Figs. 4 and 5
7 incorporated into a crawler unit 32. The unit 32
8 comprises a drive unit 33 having driven wheels 34 and a
9 control panel 35. The drive unit 33 is mechanically
10 and electrically coupled to an X-ray unit 36 in which
11 the apparatus of Figs. 4 and 5 is located. The X-rays
12 are emitted around the circumferential section 37 of
13 the unit 36. The X-ray unit 36 is coupled to a tell
14 tail unit 38 which incorporates freely rotating wheels
15 39.

16 Fig. 7 shows a battery box unit 40 for coupling to the
17 drive unit 33 for supplying power to the drive unit 33
18 and X-ray unit 36. The unit 40 has wheels 41 and a
19 retrieval ring 42 on one end.

20 Fig. 8 shows a retrieval unit 43 having a harpoon 44
21 which can engage with the retrieval ring 42. If the
22 crawler unit becomes stuck or stops within a pipe, the
23 retrieval unit 43 may be dispatched down the pipe so
24 that the harpoon 44 engages the retrieval ring 42 to
25 permit the crawler unit, comprising units 33, 36, 38,
26 40 to be retrieved from the pipe.

1 CLAIMS

2 1. A mobile X-ray unit for insertion into a tubular
3 member, the unit comprising a low voltage direct
4 current power supply; an inverter coupled to the power
5 supply, the inverter converting the low voltage direct
6 current from the power supply to alternating current;
7 rectifier means coupled to the inverter, the rectifier
8 converting the alternating current to high voltage
9 direct current; and an X-ray source coupled to the
10 rectifier to receive the high voltage direct current
11 from the rectifier to generate X-rays; and coupling
12 means to couple the unit to translation means which
13 propels the unit within the tubular member.

14
15 2. A mobile X-ray unit according to Claim 1, wherein
16 the translation means is in the form of a crawler unit
17 which propels the X-ray unit within the tubular member.

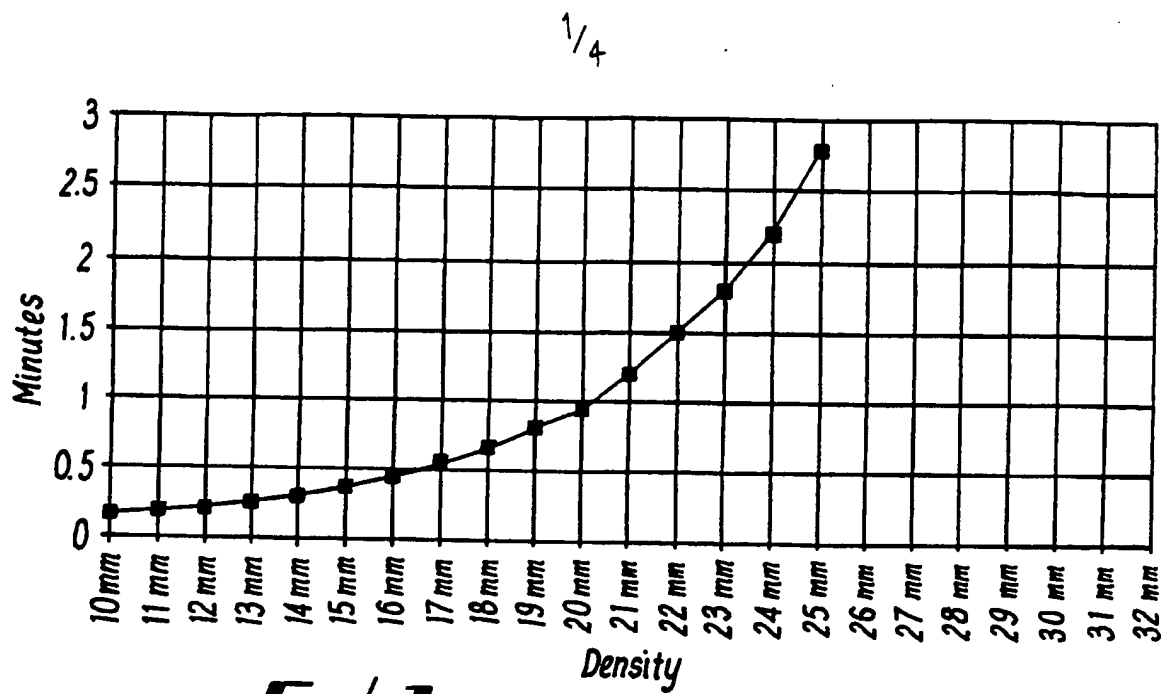
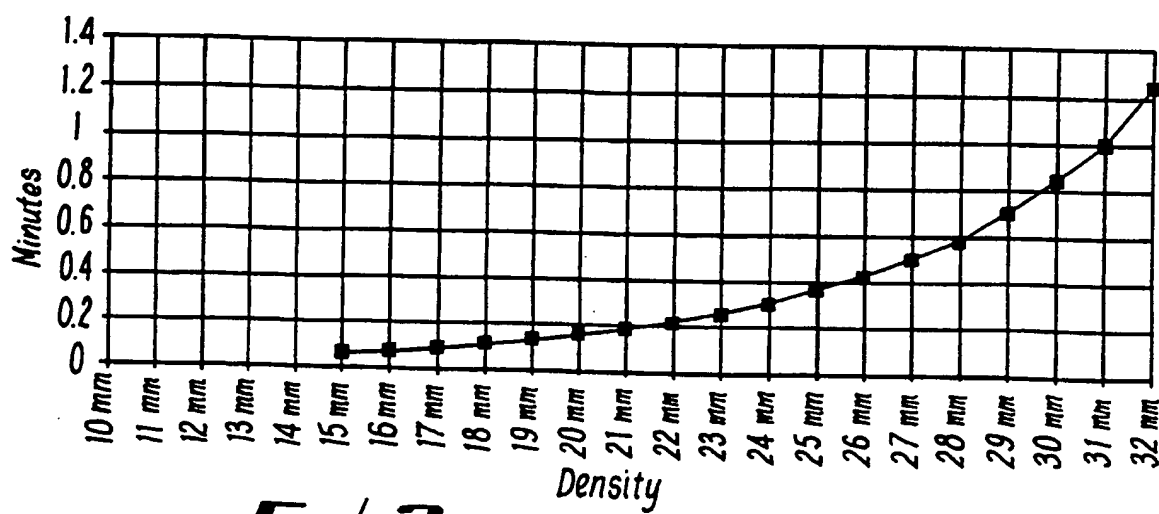
18 3. A mobile X-ray unit according to Claim 1 or Claim
19 2, wherein the power supply comprises a battery pack
20 coupled to the translation means.

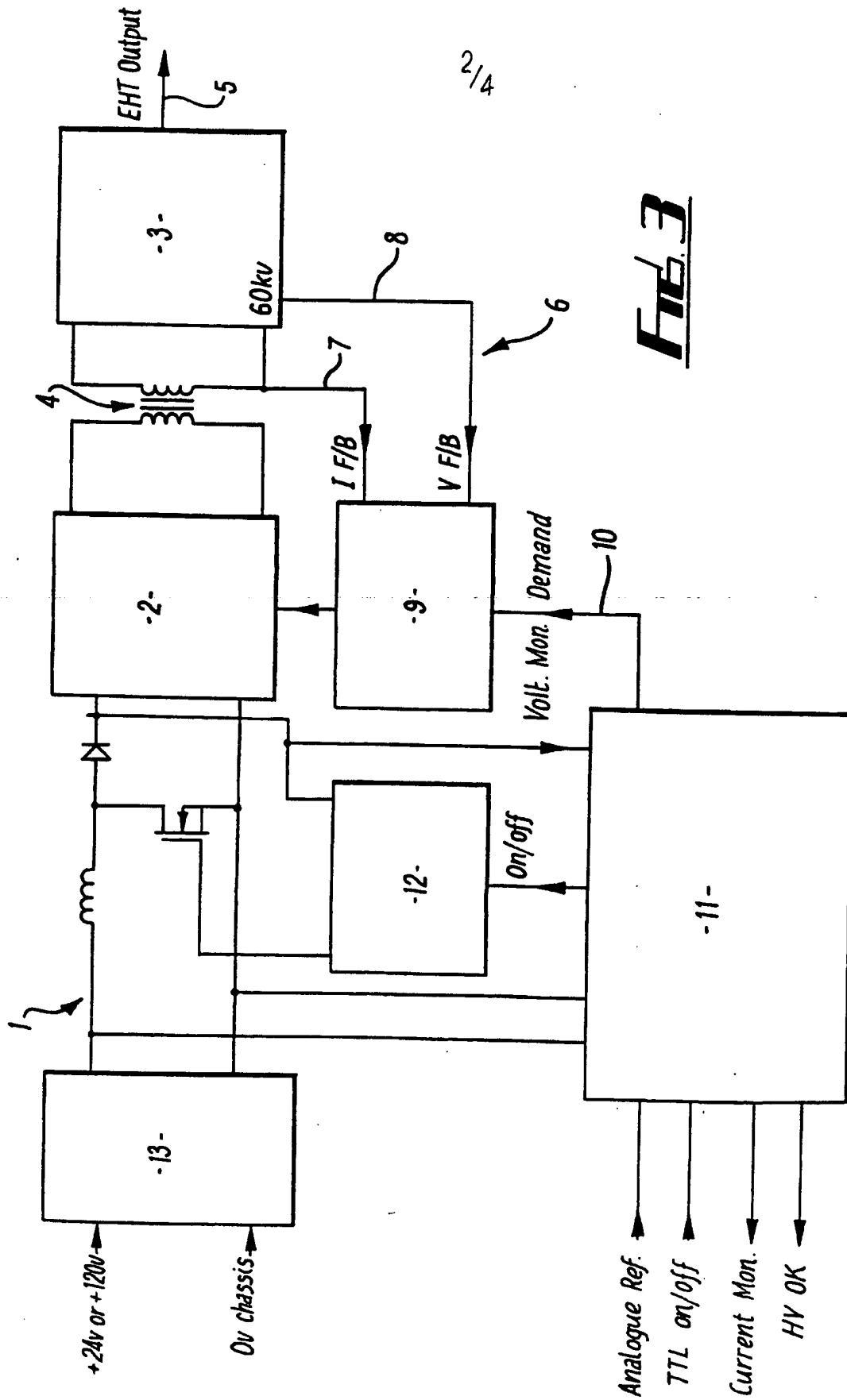
21 4. A mobile X-ray unit according to any of the
22 preceding Claims, wherein the rectifier is encapsulated
23 in an insulating solid.

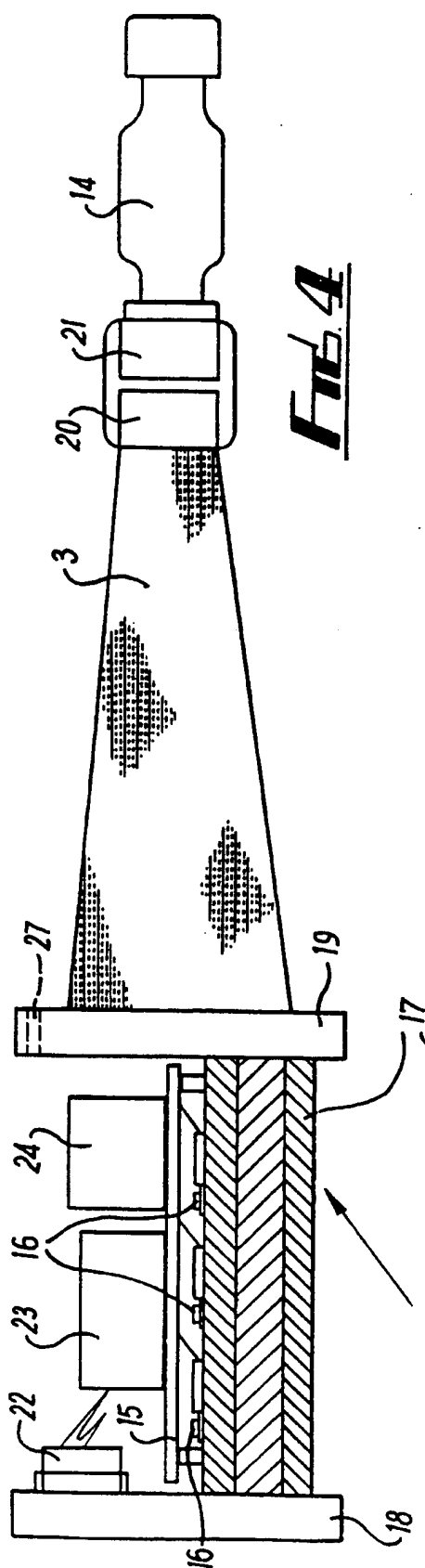
24 5. A mobile X-ray unit according to Claim 4, wherein
25 the insulating solid comprises an epoxy resin.

26 6. A mobile X-ray unit according to Claim 4 or Claim
27 5, wherein the insulating solid includes a filler
28 material to enhance the dielectric strength of the
29 insulating solid.

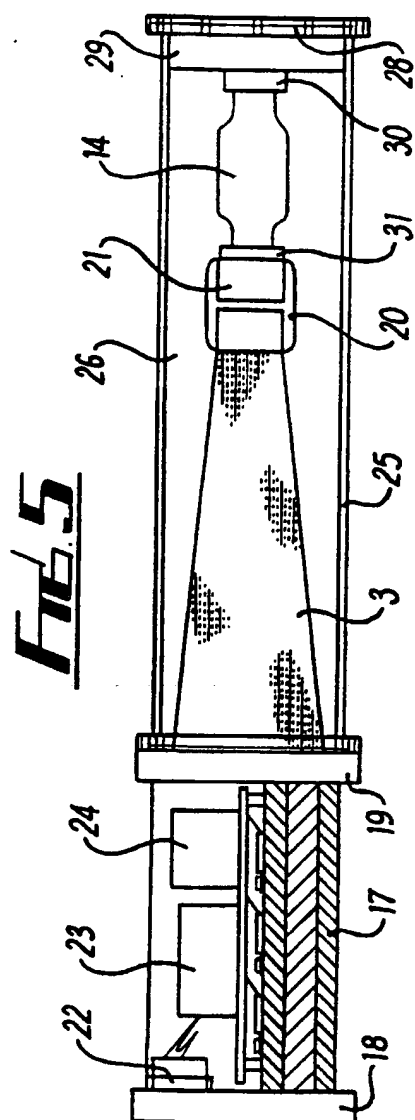
- 1 7. A mobile X-ray unit according to Claim 6, wherein
2 the filler material comprises alumina.
- 3 8. A mobile X-ray unit according to any of the
4 preceding Claims, wherein the rectifier comprises
5 diodes, capacitors and resistors arranged to form a
6 Cockroft-Walton ladder.
- 7 9. A mobile X-ray unit according to any of the
8 preceding claims, wherein the X-ray source comprises an
9 anode and a cathode, the high voltage direct current
10 being applied to the anode and the cathode is grounded.
- 11 10. A mobile X-ray unit according to Claim 9, when
12 dependent on Claim 8, wherein the diodes in the
13 Cockroft-Walton ladder are inverted.

FIG. 1FIG. 2



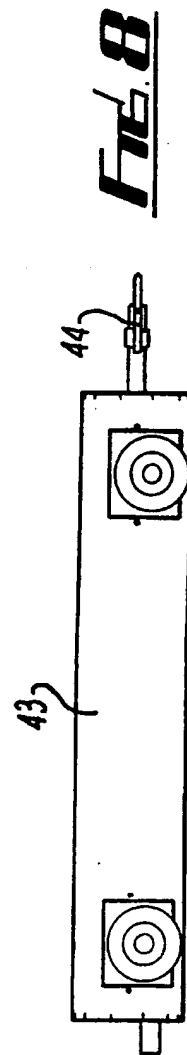
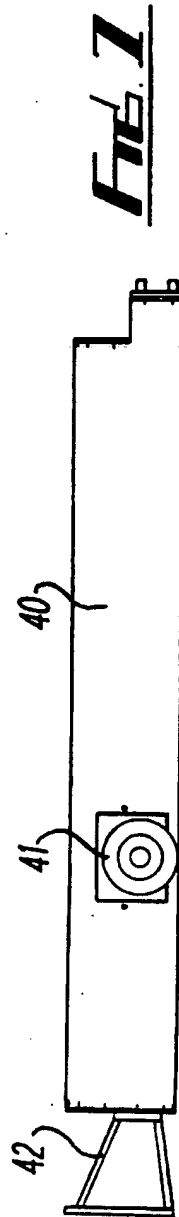
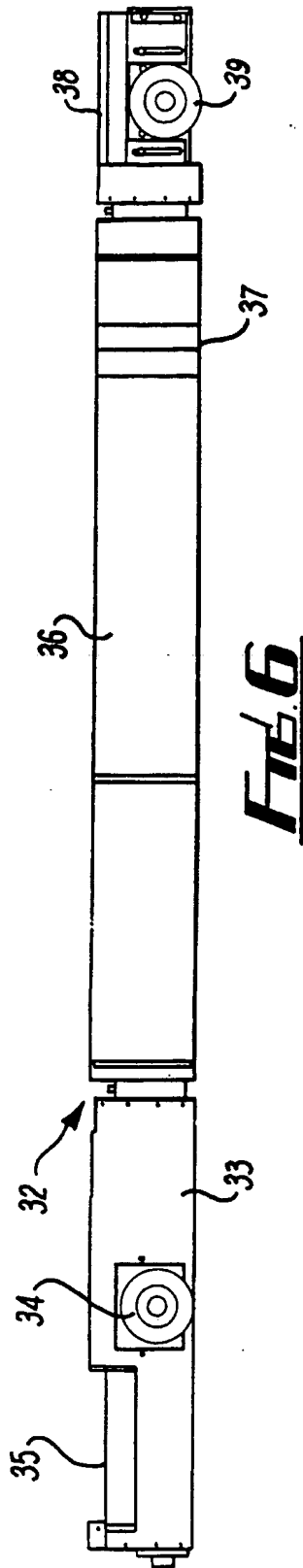


File 4



FILE 5

4/4



INTERNATIONAL SEARCH REPORT

International Application No
PCT/GB 94/02087

A. CLASSIFICATION OF SUBJECT MATTER
IPC 6 H05G1/10 G01N23/18

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 H05G G01N

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US,A,4 694 480 (B. SKILLICORN) 15 September 1987 see column 1, line 47 - column 2, line 59 see column 5, line 33 - column 6, line 57	1,2,4,9
A	---	8,10
Y	US,A,3 691 385 (T.E. KETCHBAW ET AL.) 12 September 1972 see column 1, line 3 - line 58 see column 2, line 31 - line 64	1,2
A	---	3
Y	EP,A,0 488 991 (XI TECH INC.) 3 June 1992 see abstract see column 5, line 8 - column 6, line 26 see column 11, line 31 - column 12, line 56	4,9
A	---	1
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☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

18 January 1995

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INTERNATIONAL SEARCH REPORT

International Application No

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C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US,A,3 904 878 (C.A. BURCH ET AL.) 9 September 1975 see abstract ---	1,2
A	US,A,4 797 907 (R.L. ANDERTON) 10 January 1989 see column 9, line 65 - column 10, line 49 see column 12, line 41 - column 13, line 38; figures 2,6,8 ---	1,9
A	GB,A,1 321 844 (CORROSION & WELDING ENGINEERING LIMITED) 4 July 1973 see page 1, line 33 - page 2, line 62 ---	1,2
A	EP,A,0 405 399 (KABUSHIKI KAISHA TOSHIBA) 2 January 1991 see column 11, line 42 - column 12, line 50 ---	1,4,8-10
A	US,A,5 077 771 (B. SKILLICORN ET AL.) 31 December 1991 see column 3, line 27 - column 5, line 2 ---	1,4,9
A	EP,A,0 429 315 (VARIAN ASSOCIATES, INC.) 29 May 1991 see abstract see page 7, line 46 - page 8, line 39; figures 1,3A -----	1,9

INTERNATIONAL SEARCH REPORT

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